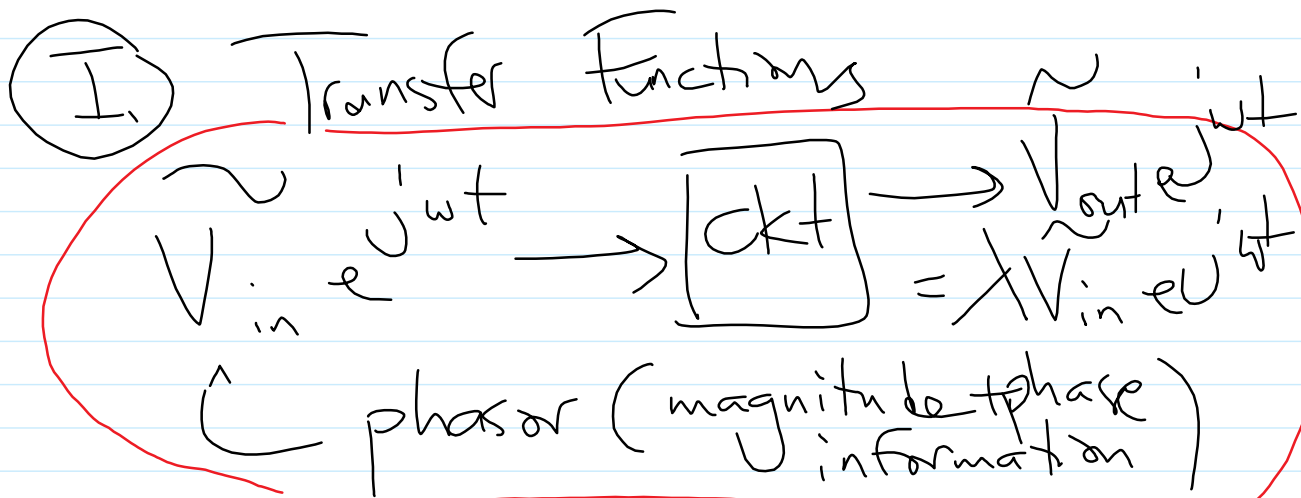


# Filters and Transfer Functions



$$A \vec{v} = \lambda \vec{v}$$

That value of  $\lambda$  is usually important!

$\Rightarrow$  new name!

transfer function

$$\frac{\tilde{V}_{out} e^{j\omega t}}{\tilde{V}_{in} e^{j\omega t}} = \frac{\tilde{V}_{out}}{\tilde{V}_{in}} = \lambda = H(j\omega)$$

$H(\omega)$  doesn't have to be

$\frac{V_{out}}{V_{in}}$  be currents  $\tilde{I}$

$\frac{\tilde{V}_{out}}{\tilde{I}_{in}}$ ,  $\frac{\tilde{I}_{out}}{\tilde{I}_{in}}$ ,  $\frac{\tilde{I}_{out}}{\tilde{V}_{in}}$

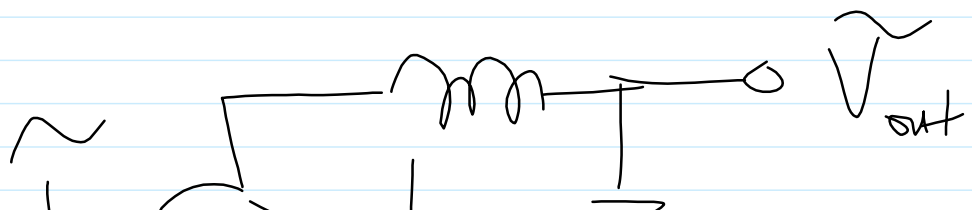
$\frac{\tilde{V}}{\tilde{I}} = Z$  ← impedance!

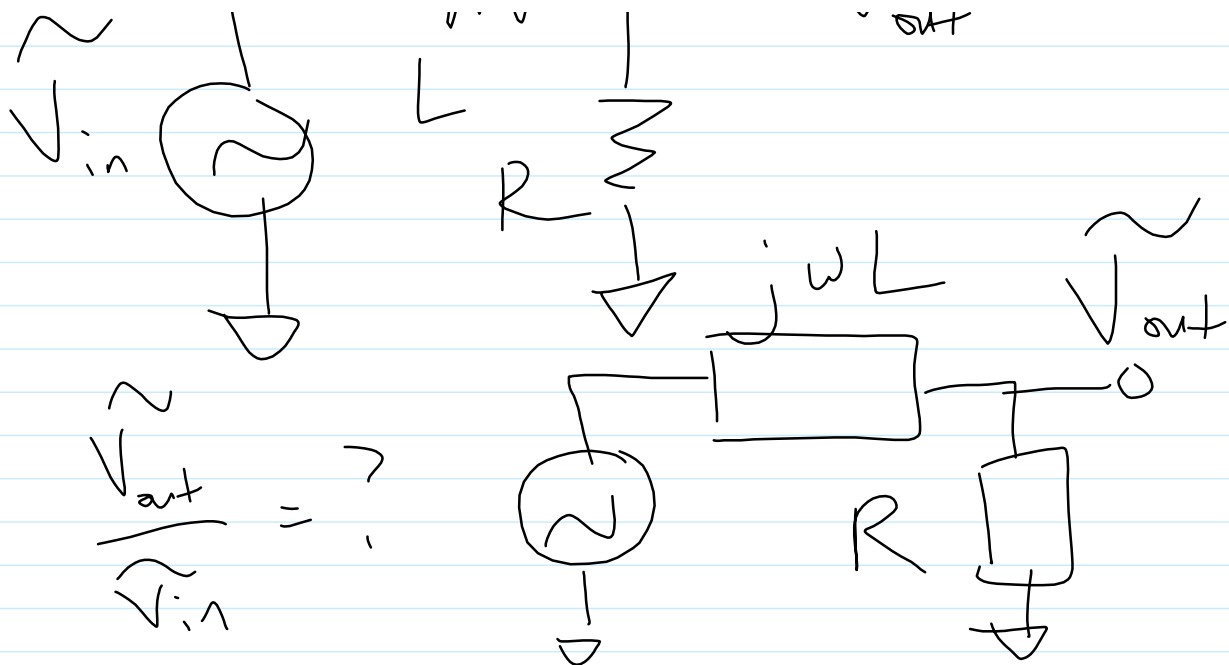
Impedance expression ( $Z_L = j\omega L, Z_C = \frac{1}{j\omega C}$ )

↳ another form of transfer fn

How do you calculate  $H(\omega)$ ?

⇒ IBA circuit analysis, resistors → impedances





$$\frac{V_{out}}{V_{in}} = ?$$

$$V_{out} = \frac{Z_R}{Z_R + Z_L} V_{in}$$

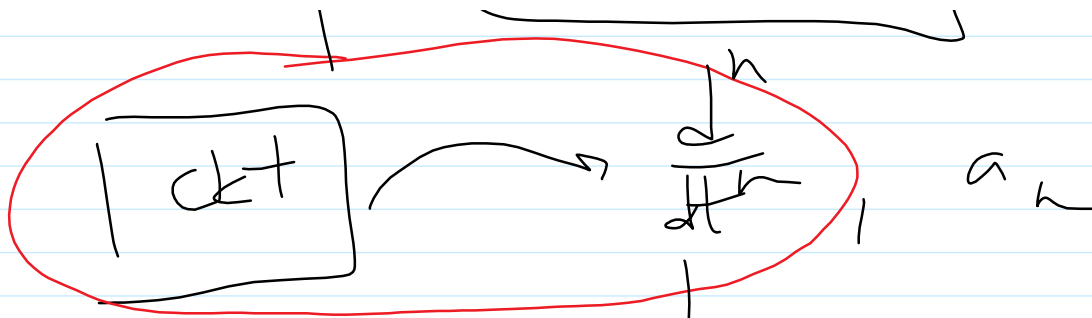
$$\Rightarrow H(j\omega) = \frac{V_{out}}{V_{in}} = \frac{Z_R}{Z_R + Z_L} = \frac{R}{R + j\omega L}$$

## Recap of D3 2B

Care about sinusoidal inputs

↳ to simplify analysis,

$$v(t) = V_0 \cos(\omega t + \phi) = \text{Re} \left\{ \underbrace{V_0 e^{j\phi}}_{\text{phasor}} e^{j\omega t} \right\}$$



$$(j\omega)^n \left( \frac{a_n}{(j\omega)^n} \right)$$

this is a constant relative to  $\omega$

### Some comments on $H(j\omega)$

\* complex-valued: has both a magnitude and phase

$$|H(j\omega)|$$

$$\angle H(j\omega)$$

\* frequency dependent

↳ so you can think of  $H(j\omega)$  kind of like

a frequency-dependent gain  
⇒ recall in 16 A!

$$A = \frac{V_{out}}{V_{in}} \quad \text{for an op-amp}$$

Sinusoidal input:

$$\Rightarrow \cos(\omega t) \text{ or } \sin(\omega t) \\ \text{or } \cos(\omega_1 t) + \cos(\omega_2 t) + \dots$$

$$\cos(\omega t) = \operatorname{Re}\{e^{j\omega t}\}$$

\*\*\*

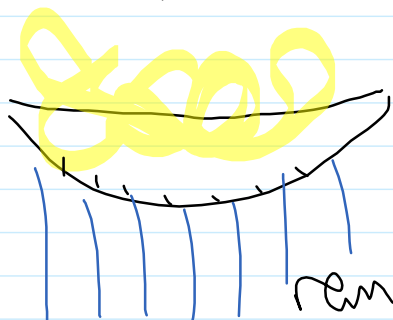
Using  $e^{j\omega t}$  instead of  $\operatorname{Re}\{e^{j\omega t}\} = \cos(\omega t)$  makes the math easier

$$V_o e^{j\omega t} \longrightarrow V_o \cos(\omega t + \phi)$$

Corresponds to

II, Filters

pasta

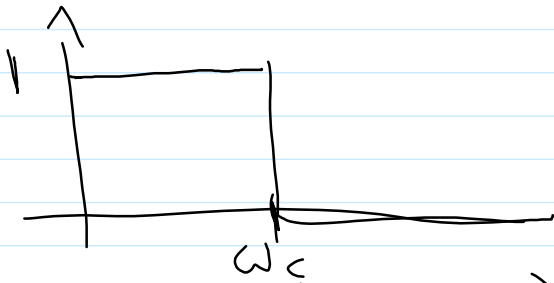


: given a signal,  
we would like to  
remove certain parts

(e.g. high freq. noise)

⇒ part of bigger field  
called signal processing

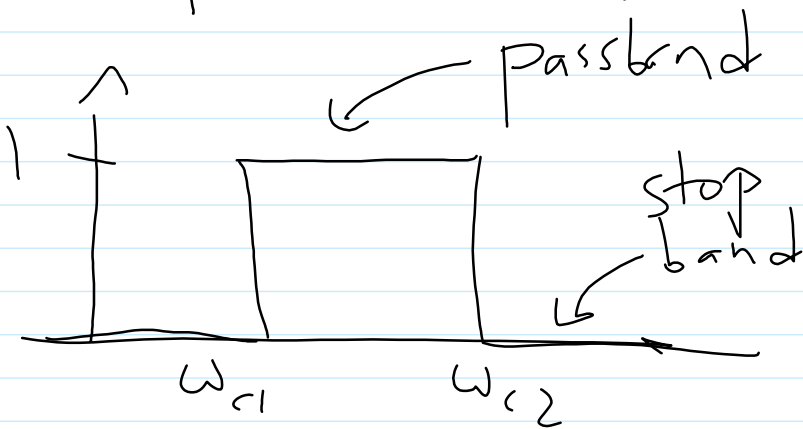
## Ideal Filters



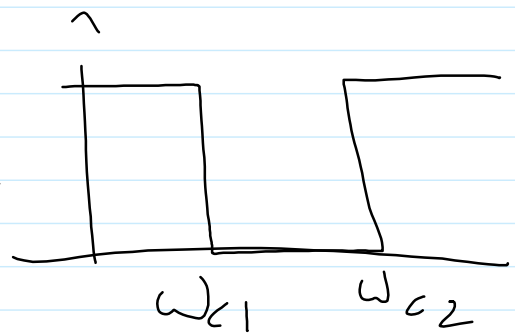
low pass (LPF)



high pass (HPF)



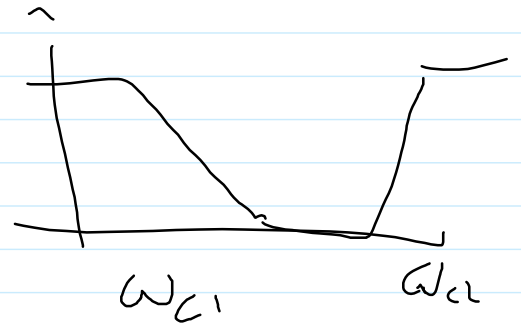
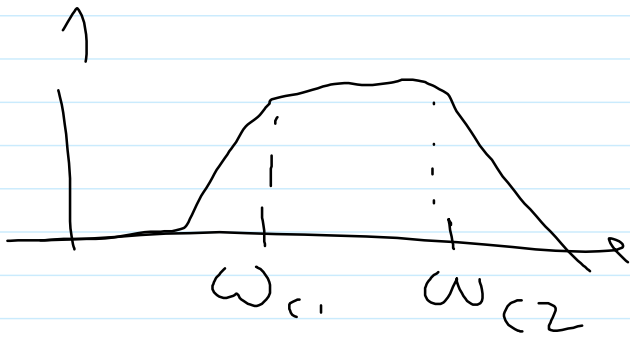
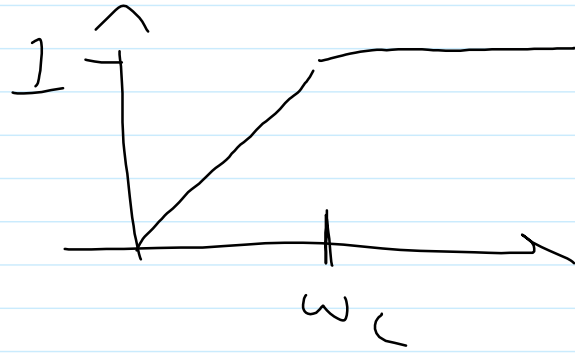
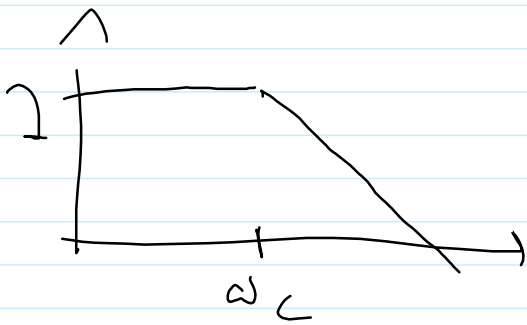
bandpass



bandstop

In practice, never going to get  
sharp edges " " " "

→ same roll off



How do we actually implement this?

- digital filtering (software)

→ take EE123

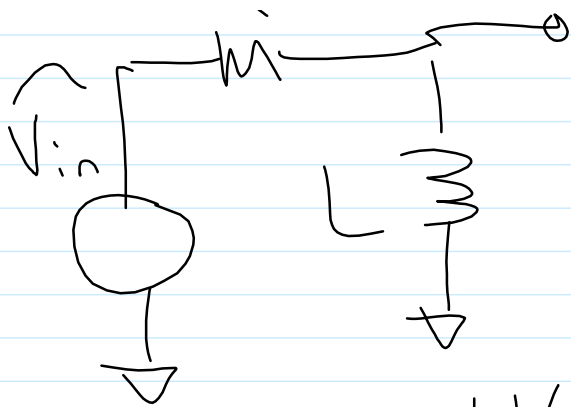
- analog filtering

→ circuit → Transfer fn!

$H(j\omega)$  does some freq-dependent

Scaling of input signal





$$H(j\omega) = \frac{j\omega L}{j\omega L + R}$$

stop LF  $\rightarrow H(j0) = \frac{0}{0+R} = 0$

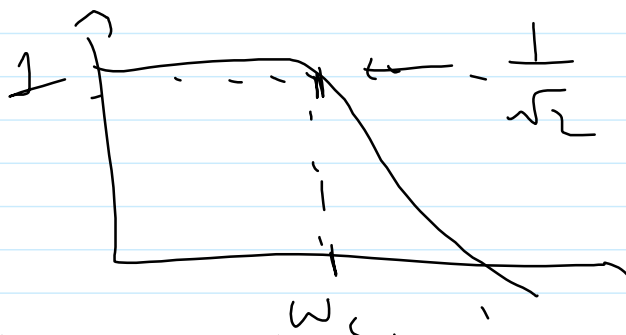
keep HF  $H(j\infty) = \frac{j\omega L}{j\omega L} = 1$

$\Rightarrow$  high pass filter

\* Cutoff/Corner Frequency

— common definition:

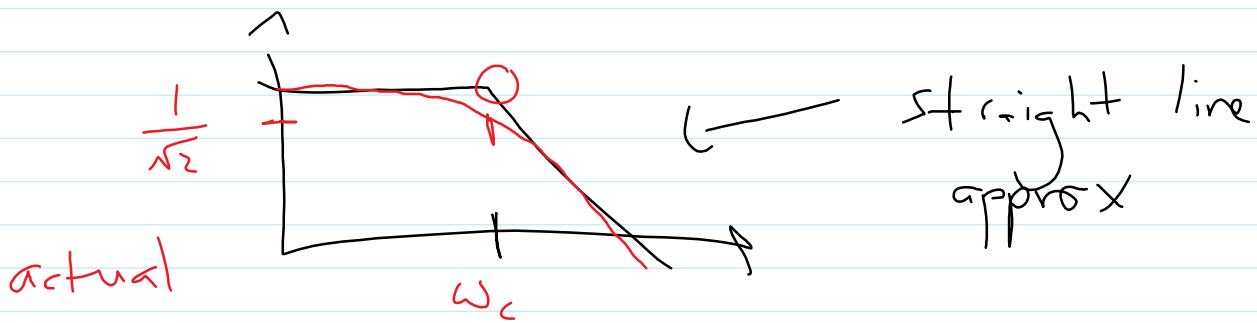
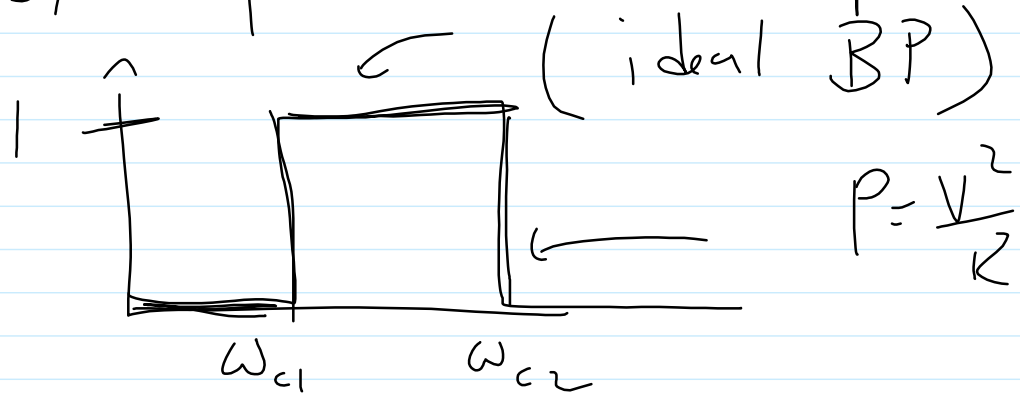
when the  $|H(j\omega)|$  is  $\frac{1}{\sqrt{2}}$  of the value at the passband



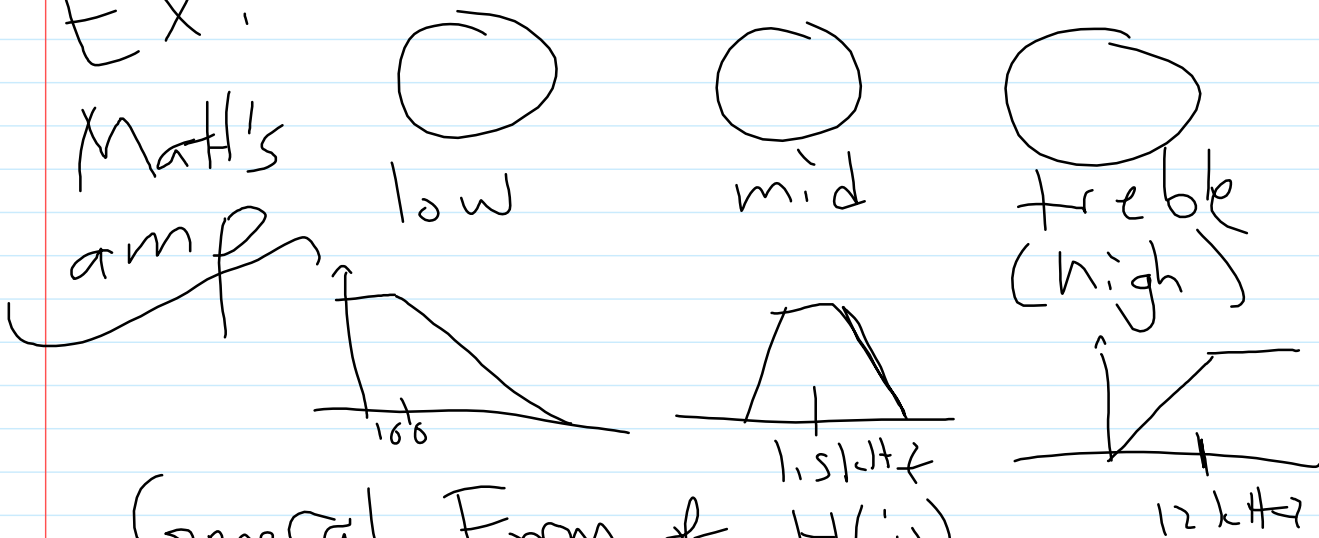
— intuitive definition: when there's



a "cutoff", i.e., a boundary  
b/w passband and stopband

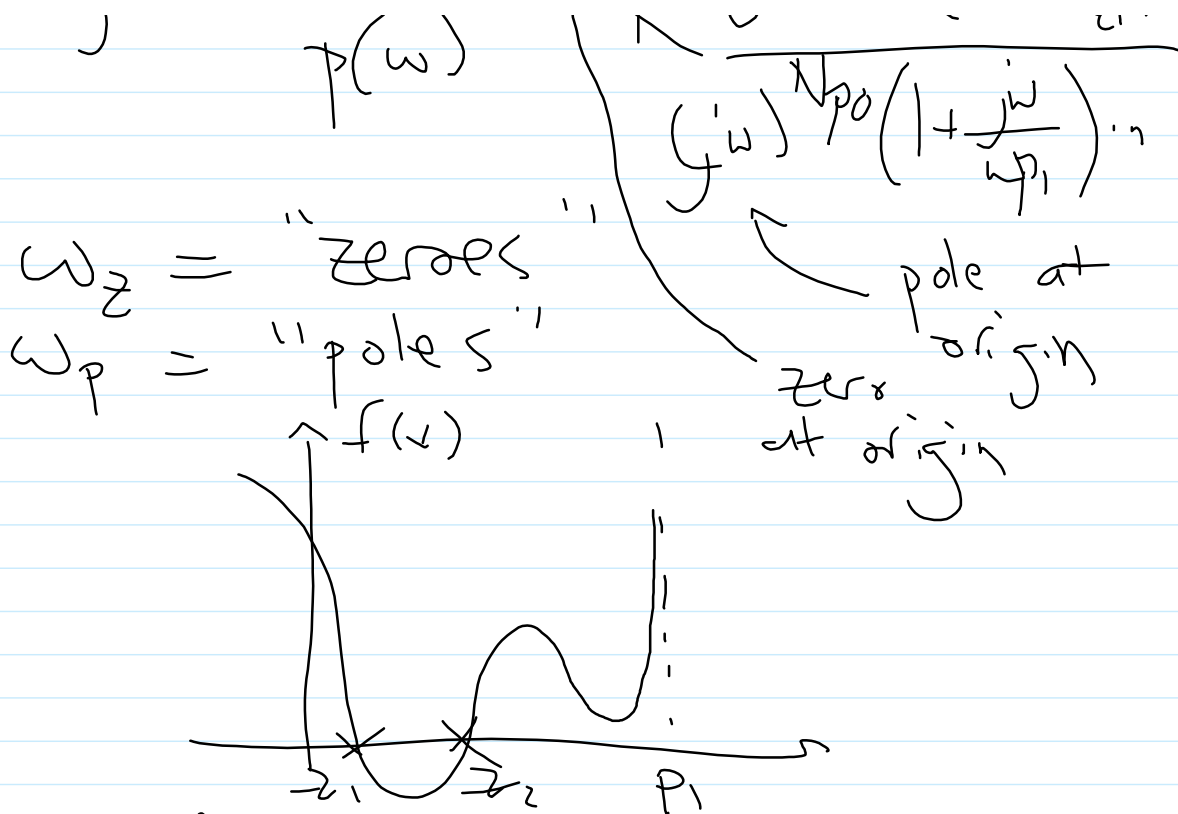


EX: 100 Hz 1.5 kHz 12 kHz



General Form of  $H(j\omega)$

$$H(j\omega) = \frac{Z(\omega)}{P(\omega)} = K \frac{(j\omega)^{N_{z0}} (1 + \frac{j\omega}{\omega_{z1}}) \dots}{\dots (N_{p0}/1 \dots \omega \dots)}$$



zeros of  $f(x)$  are values  $z$  s.t.

$$f(z) = 0$$

poles of  $f(x)$  are values  $p$  s.t.

$$f(p) = \infty$$

$$H(j\omega) = \frac{\left(1 + \frac{j\omega}{\omega_{z1}}\right) \left(1 + \frac{j\omega}{\omega_{z2}}\right) \dots}{\left(1 + \frac{j\omega}{\omega_{p1}}\right) \left(1 + \frac{j\omega}{\omega_{p2}}\right) \dots}$$

$$\begin{aligned}
 s &= j\omega \\
 &= \frac{\left(1 + \frac{s}{\omega_{z1}}\right) \dots}{\left(1 + \frac{s}{\omega_{p1}}\right) \dots}
 \end{aligned}$$

$$\overline{\left(1 + \frac{s}{\omega_{p1}}\right) \dots}$$

Then, we see that  $s = -\omega_{p1}$   
is what sends  $H(j\omega) \rightarrow \infty$

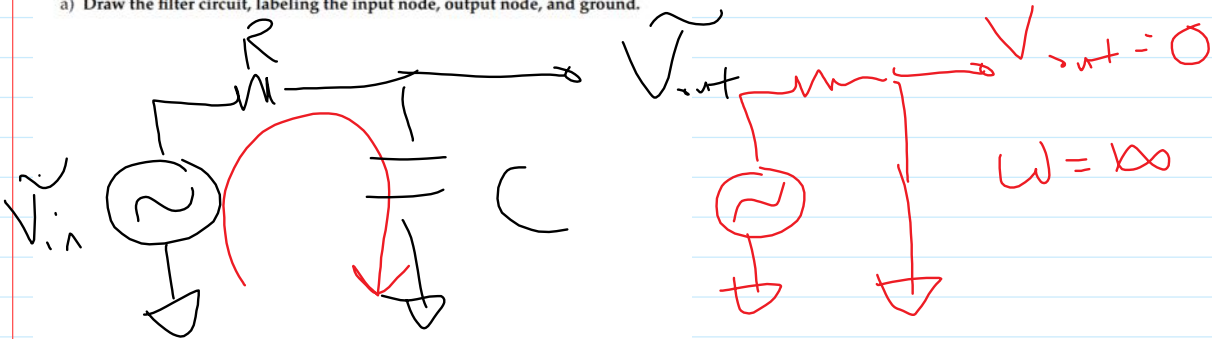
and  $s = -\omega_{z1}$   
is what sends  $H(j\omega) \rightarrow 0$

# Dis 2C Worksheet

Wednesday, July 1, 2020 12:57 PM

You have a 1 kΩ resistor and a 1 μF capacitor wired up as a low-pass filter.

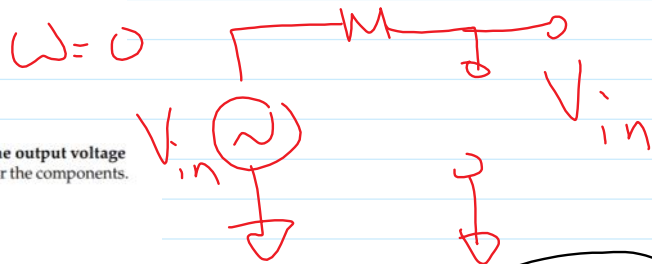
a) Draw the filter circuit, labeling the input node, output node, and ground.



$$Z_c(\omega) = \frac{1}{j\omega C} \quad ; \quad \omega \rightarrow 0 : \text{open}$$

$$\omega \rightarrow \infty : \text{short}$$

$$V = ZI$$



b) Write down the transfer function of the filter,  $H(j\omega)$  that relates the output voltage phasor to the input voltage phasor. Be sure to use the given values for the components.

$$H(j\omega) = \frac{j\omega C}{R + \frac{1}{j\omega C}} = \frac{1}{1 + j\omega RC} = \frac{1}{1 + \frac{j\omega}{10^3}}$$

$$RC = 1 \text{ k}\Omega \times 1 \mu\text{F} = 10^{-3} \text{ s}$$

$$= \frac{1}{(1 + \frac{j\omega}{\omega_p})}$$

c) Write an exact expression for the magnitude of  $H(j\omega = j10^2)$ , and give an approximate numerical answer.

$$|H(j\omega)| = \left| \frac{1}{1 + \frac{j\omega}{\omega_p}} \right|$$

$$= \frac{1}{\sqrt{1^2 + \left(\frac{\omega}{\omega_p}\right)^2}} = \frac{1}{\sqrt{1 + \left(\frac{10^2}{10^3}\right)^2}}$$

$\omega_p = 10^3 \text{ rad/s}$

$z = x + jy$

$|z| = \sqrt{x^2 + y^2}$

$$|H(j10^2)| = \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_p}\right)^2}} \approx \frac{1}{\sqrt{1 + \left(\frac{10^2}{10^3}\right)^2}}$$

$$= |z_1| |z_2|$$

$$|H(j10^2)| \approx 1$$

Specifically, for  $\omega \ll \omega_p$ ,  $\left(\frac{\omega}{\omega_p}\right)^2 \ll 1$

$$\Rightarrow |H(j\omega \ll j\omega_p)| \approx \frac{1}{\sqrt{1}} = 1$$

d) Write an exact expression for the magnitude of  $H(j\omega = j10^6)$ , and give an approximate numerical answer.

$$|H(j10^6)| = \frac{1}{\sqrt{1 + \left(\frac{10^6}{10^3}\right)^2}} = \frac{1}{\sqrt{1 + 10^6}}$$

$$|H(j10^6)| \approx \frac{1}{\sqrt{10^6}} = \frac{1}{10^3} = 10^{-3}$$

Specifically, for  $\omega \gg \omega_p$ ,  $\left(\frac{\omega}{\omega_p}\right)^2 \gg 1$

e) Write an exact expression for the phase of  $H(j\omega = j1)$ , and give an approximate numerical answer.

$$H(j\omega) = \frac{1}{1 + j\frac{\omega}{\omega_p}}$$

$$\Rightarrow |H| = \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_p}\right)^2}}$$

$$\approx \frac{1}{\sqrt{\left(\frac{\omega}{\omega_p}\right)^2}} = \frac{\omega_p}{\omega}$$

$$\angle \left(\frac{z_1}{z_2}\right) = \angle z_1 - \angle z_2$$

$$\angle \frac{|z_1| e^{j\theta_1}}{|z_2| e^{j\theta_2}} = \angle e^{j(\theta_1 - \theta_2)}$$

$$= \theta_1 - \theta_2$$

$$= \angle z_1 - \angle z_2$$

$$z_1 z_2$$

$$= z_1 - z_2$$

$$\angle z_1 z_2 = \angle z_1 + \angle z_2 \quad z = x + jy$$

$$\angle \frac{1}{1 + \frac{j\omega}{\omega_p}} = \angle 1 - \angle \left( 1 + \frac{j\omega}{\omega_p} \right)$$

$$= - \angle \left( 1 + \frac{j\omega}{\omega_p} \right) = - \arctan \left( \frac{\omega}{\omega_p} / 1 \right)$$

$$\angle H(j\omega) = - \arctan \left( \frac{1}{10^3}, 1 \right)$$

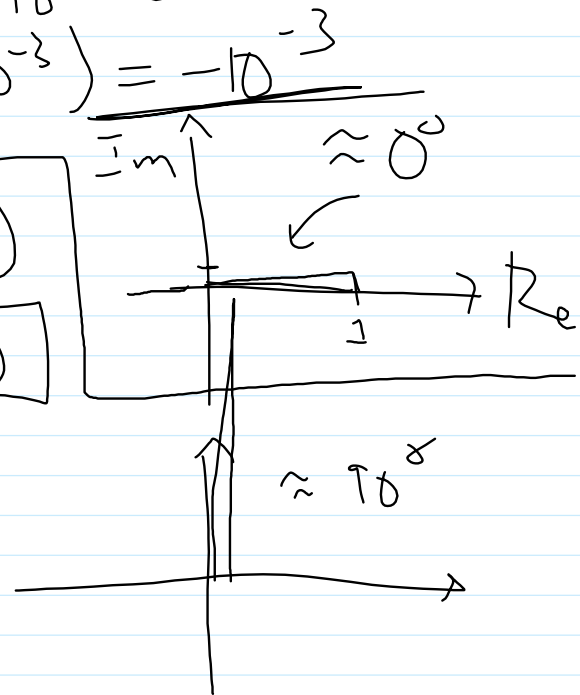
$$= - \arctan(10^{-3}) = -10^{-3}$$

f) Write an exact expression for the phase of  $H(j\omega = j10^6)$ , and give an approximate numerical answer.

$$\angle H(j\omega) = - \arctan \left( \frac{10^6}{10^3}, 1 \right)$$

$$= - \arctan(10^3, 1)$$

$$\approx -90^\circ$$

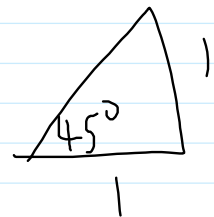


g) Write down an expression for the corner frequency  $\omega_c$  of this circuit. Evaluate the magnitude and phase of  $H(j\omega_c)$ .

$$\frac{1}{\sqrt{2}} = |H(j\omega_c)| = \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_p}\right)^2}}$$

$$\Rightarrow \omega_c = \omega_p = 10^3 \text{ rad/s}$$

$$|H(j\omega_c)| = \frac{1}{\sqrt{2}}$$



$$\angle H(j\omega_c) = - \arctan \left( \frac{\omega_c}{\omega_c}, 1 \right)$$

$$= -\frac{11}{4} = -45^\circ$$

h) Write down an expression for the time-domain output waveform  $V_{out}(t)$  of this filter if the input voltage is  $V(t) = 1 \sin(1000t)$  V. You can assume that any transients have died out — we are interested in the steady-state waveform.

$$\omega = 10^3 \text{ rad/s}$$

$$= \omega_c$$

$$V(t) = 1 \sin(1000t)$$

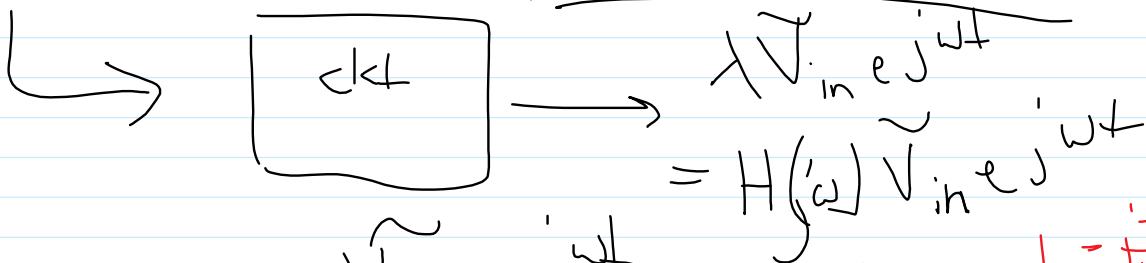
$$V_{out}(t) = 1 \cos\left(1000t - \frac{\pi}{2}\right)$$

By convention,

$$\tilde{V}_o = V_o e^{j\phi} \text{ where}$$

$$\text{Re}\{\tilde{V}_o e^{j\omega t}\} = V_o \cos(\omega t + \phi)$$

$$= \frac{1}{2} \left( e^{j\omega t} e^{-j\frac{\pi}{2}} + e^{-j\omega t} e^{j\frac{\pi}{2}} \right)$$



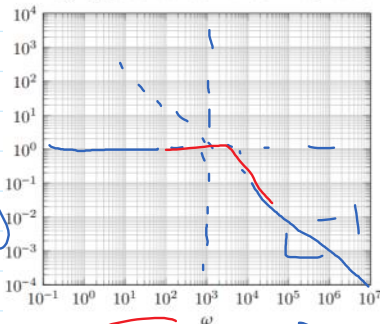
$$H(j\omega) = \frac{V_{out} e^{j\omega t}}{V_{in} e^{j\omega t}} \Rightarrow H(j\omega_c) = \frac{1}{\sqrt{2}} e^{-j\frac{\pi}{4}}$$

$$H(j\omega_c) \tilde{V}_{in} = \frac{1}{\sqrt{2}} e^{-j\frac{\pi}{4}} e^{-j\frac{\pi}{2}} = \frac{1}{\sqrt{2}} e^{-j\frac{3\pi}{4}} = V_{out}$$

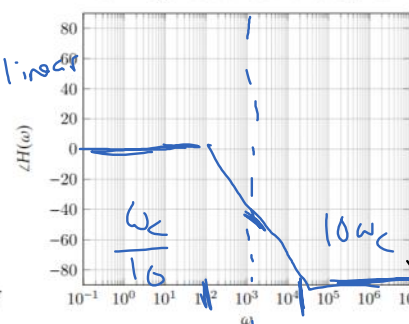
convert back to time domain

i) Based off the values calculated in the previous parts, predict what the Bode plots (both magnitude and phase) of the filter will look like and sketch them on the graph paper below. You may use a straight line approximation.

Log-log plot of transfer function magnitude



Semi-log plot of transfer function phase



j) Use a computer to draw the Bode plots (both magnitude and phase) of the filter. Compare them to your sketch from before.

$$V_{out}(t) = \frac{1}{\sqrt{2}} \cos\left(\omega t - \frac{3\pi}{4}\right)$$

j) Use a computer to draw the Bode plots (both magnitude and phase) of the filter. Compare them to your sketch from before.

$$V_{out} = \frac{1}{\sqrt{2}} \sin\left(\omega t - \frac{\pi}{4}\right)$$

$$\omega \ll \omega_c: |H| \approx 1$$

$$\omega \gg \omega_c: |H| \approx \frac{\omega_c}{\omega}$$

$$\omega \ll \omega_c: \angle H \approx 0$$

$$\omega \gg \omega_c: \angle H \approx -90^\circ \quad \angle H(\omega_c) = -45^\circ$$

$$\omega = \frac{\omega_c}{10}: \angle H\left(j\frac{\omega_c}{10}\right) = -\arctan\left(\frac{\frac{\omega_c}{10}}{1}\right) = -\arctan\left(\frac{1}{10}\right) \approx -0.1 \text{ rad} \approx -6^\circ$$



$$\omega = 10\omega_c: \angle H(j10\omega_c) = -\arctan(10) = -84^\circ$$

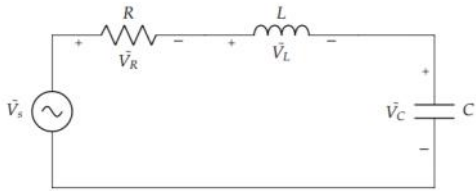
$$\omega = 2\pi f \implies f = \frac{\omega}{2\pi}$$

$$"2\pi = 10"$$

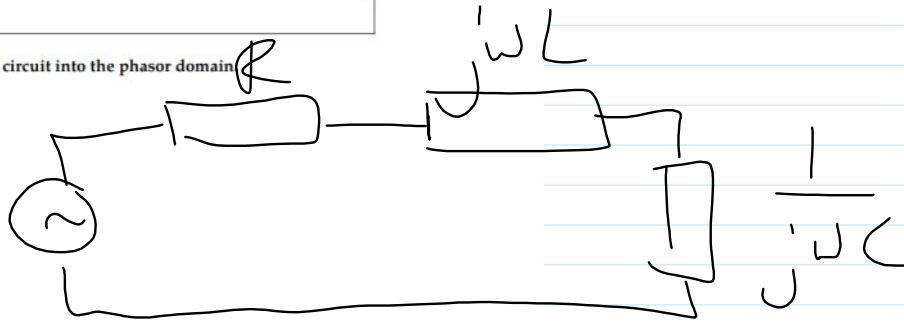


### 3 RLC Circuit

In this question, we will take a look at an electrical systems described by second-order differential equations and analyze it in the phasor domain. Consider the circuit below where  $\bar{V}_s$  is a sinusoidal signal,  $L = 1 \text{ mH}$ , and  $C = 1 \text{ nF}$ :



a) Transform the circuit into the phasor domain



b) Solve for the transfer function  $H_C(\omega) = \frac{\bar{V}_C}{\bar{V}_s}$  in terms of  $R$ ,  $L$ , and  $C$ .

$$H_C(\omega) = \frac{Z_C}{Z_R + Z_L + Z_C} = \frac{\frac{1}{j\omega C}}{R + j\omega L + \frac{1}{j\omega C}}$$

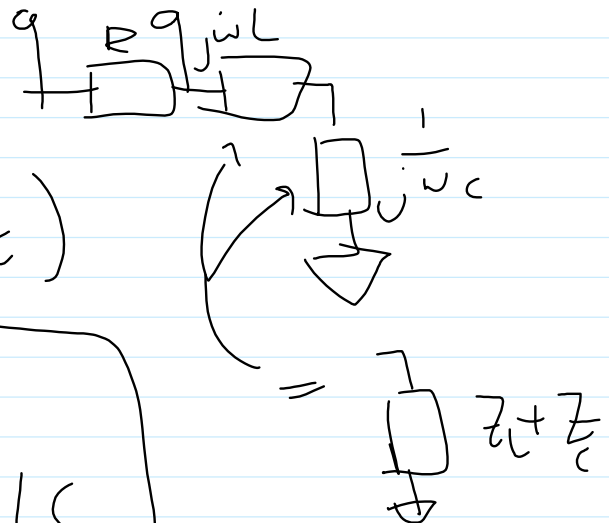
$$= \frac{1}{1 + j\omega RC + (j\omega)^2 LC}$$

c) Solve for the transfer function  $H_L(\omega) = \frac{V_L}{V_s}$  in terms of  $R$ ,  $L$ , and  $C$ .

$$\begin{aligned}
 H_L(\omega) &= \frac{Z_L}{Z_R + Z_L + Z_C} \\
 &= \frac{j\omega L}{R + j\omega L + \frac{1}{j\omega C}} \times \frac{j\omega C}{j\omega C} \\
 &= \boxed{\frac{(j\omega)^2 LC}{1 + j\omega RC + (j\omega)^2 LC}}
 \end{aligned}$$

d) Solve for the transfer function  $H_R(\omega) = \frac{V_R}{V_s}$  in terms of  $R$ ,  $L$ , and  $C$ .

$$H_R(\omega) = \frac{R}{R + (j\omega L + \frac{1}{j\omega C})}$$



$$\boxed{H_R(j\omega) = \frac{j\omega RC}{1 + j\omega RC + (j\omega)^2 LC}}$$

$$H_R(j\omega) = \frac{1}{1 + j\omega RC + (j\omega)^2 LC}$$

$$\frac{1}{1 + j\omega RC + (j\omega)^2 LC}$$

e) Use a computer to draw the magnitude Bode plots of  $H_C(\omega)$ ,  $H_L(\omega)$ , and  $H_R(\omega)$  when  $R = 2 \text{ k}\Omega$ .

$$R = 2 \text{ k}\Omega, L = 1 \text{ mH}, C = 1 \text{ nF}$$

$$LC = 10^{-12} \text{ [s}^2\text{]}$$

$$RC = 2 \times 10^{-6} \text{ [s]}$$

$$I. H_R(\omega) = \frac{j\omega(2 \times 10^{-6})}{1 + j\omega(2 \times 10^{-6}) + (j\omega)^2(10^{-12})}$$

Look at how  $H(\omega)$  approaches limits.

$$\omega \rightarrow 0$$

$$\omega \rightarrow \infty$$

$$\lim_{\omega \rightarrow 0} \frac{j\omega RC}{1 + j\omega RC + (j\omega)^2 LC} = \frac{j\omega RC}{1 + 0 + 0} = j\omega RC$$

$$\omega \rightarrow 0 \quad | + j\omega RC + (j\omega)^2 LC | \approx 1 + 0 + 0 = 1$$

$$= j\omega (2 \times 10^{-6})$$

$$\lim_{\omega \rightarrow \infty} \frac{j\omega RC}{| + j\omega RC + (j\omega)^2 LC |} = \frac{j\omega RC}{(j\omega)^2 LC}$$

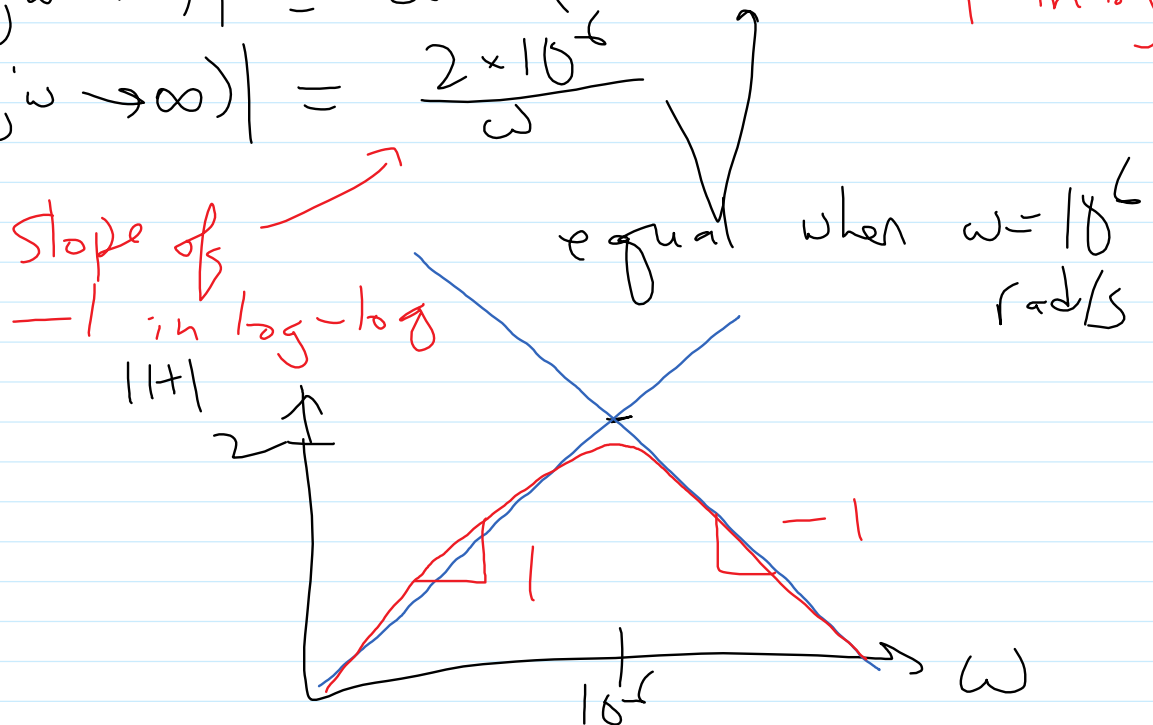
dominates

$$= \frac{R}{L} \frac{1}{j\omega} = \frac{2 \times 10^6}{1 \text{ mH}} \frac{1}{j\omega} = \frac{2 \times 10^6}{j\omega}$$

$$|H(j\omega \rightarrow 0)| = \omega \times (2 \times 10^6)$$

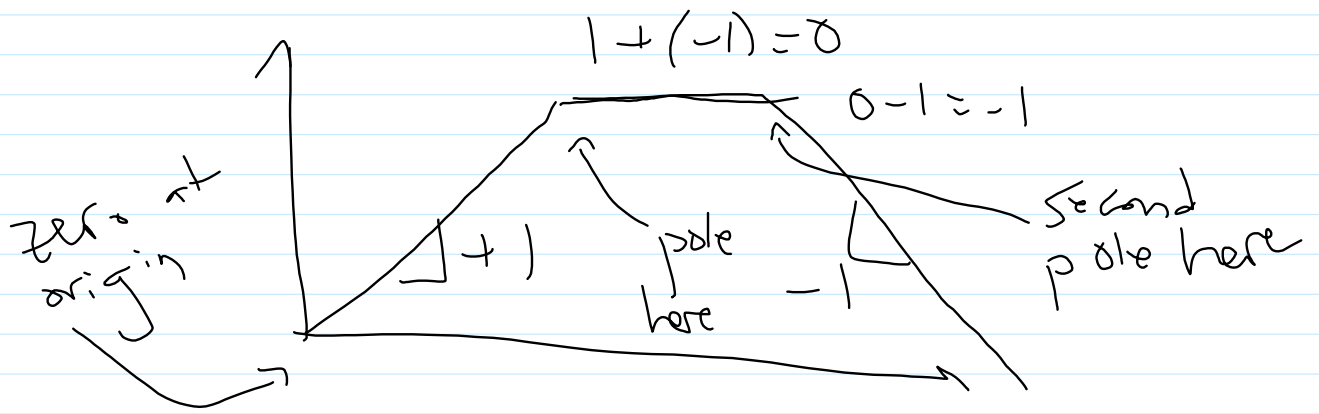
$$|H(j\omega \rightarrow \infty)| = \frac{2 \times 10^6}{\omega}$$

← slope of 1 in log-log



Tomorrow:

pole  $\rightarrow$  -1 in slope  
 zero  $\rightarrow$  +1 in slope  
 $1 + (-1) = 0$



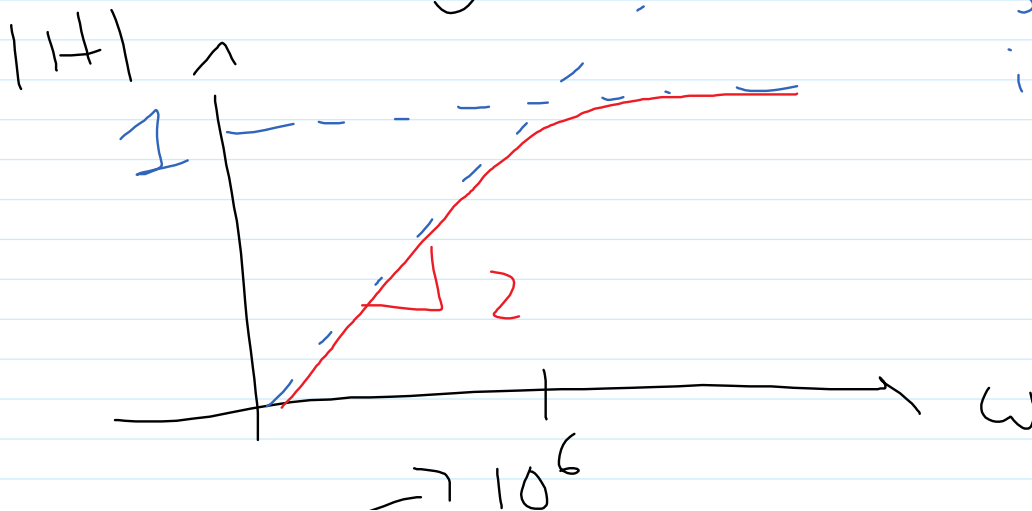
II,  $H_L(j\omega)$

$$\Rightarrow H_L(j\omega) = \frac{(j\omega)^2 LC}{1 + j\omega RC + (j\omega)^2 LC}$$

$$\lim_{\omega \rightarrow 0} H_L(\omega) = \frac{(j\omega)^2 LC}{1 + 0 + 0^2} = (j\omega)^2 LC = -\omega^2 LC = -10^{-12} \omega^2$$

$$\lim_{\omega \rightarrow \infty} H_L(\omega) = \frac{(j\omega)^2 LC}{(j\omega)^2 LC} = 1$$

slope 2  
in log-log



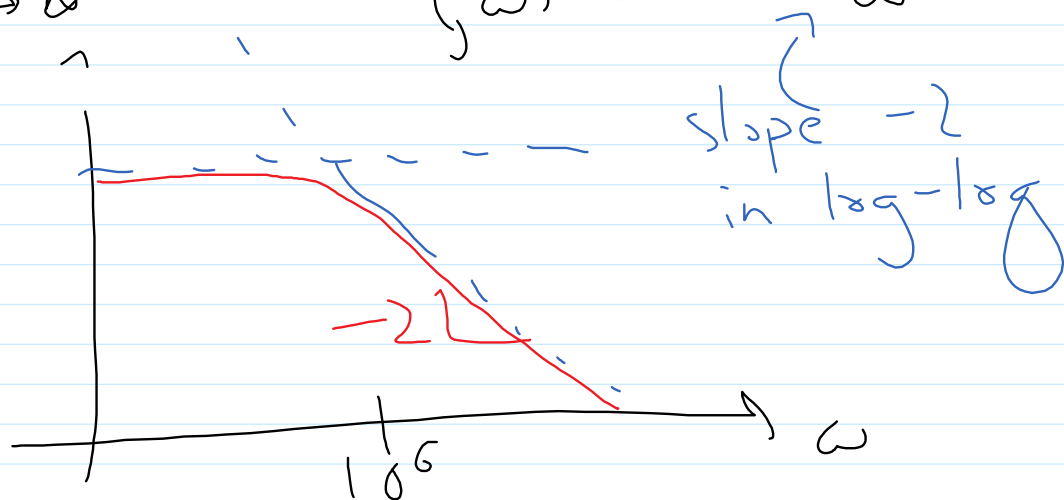
$$10^{-12} \omega^2 = 1 \quad \text{when } \omega = 10^6 \text{ rad/s}$$

III.  $H_C(\omega)$

$$\Rightarrow H_C(\omega) = \frac{1}{1 + j\omega RC + (j\omega)^2 LC}$$

$$\lim_{\omega \rightarrow 0} H_C(\omega) = \frac{1}{1 + 0 + 0} = 1$$

$$\lim_{\omega \rightarrow \infty} H_C(\omega) = \frac{1}{(j\omega)^2 LC} = \frac{-10^{12}}{\omega^2}$$



$$\frac{10^{12}}{\omega^2} = 1 \quad \text{when } \omega = 10^6 \text{ rad/s}$$