

Bode Plots

* Transfer Function Recap

* Bode plots; Intro

* Drawing Bode Plots

* Reading Bode plots

(I) Transfer Functions

$$H(\omega) = K \frac{(j\omega)^{N_{z0}} \underbrace{\left(1 + j\frac{\omega}{\omega_{z1}}\right) \left(1 + j\frac{\omega}{\omega_{z2}}\right) \dots \left(1 + j\frac{\omega}{\omega_{zn}}\right)}_{\text{zeros}}}{\underbrace{\left(1 + j\frac{\omega}{\omega_{p1}}\right) \left(1 + j\frac{\omega}{\omega_{p2}}\right) \dots \left(1 + j\frac{\omega}{\omega_{pm}}\right)}_{\text{poles}}}$$

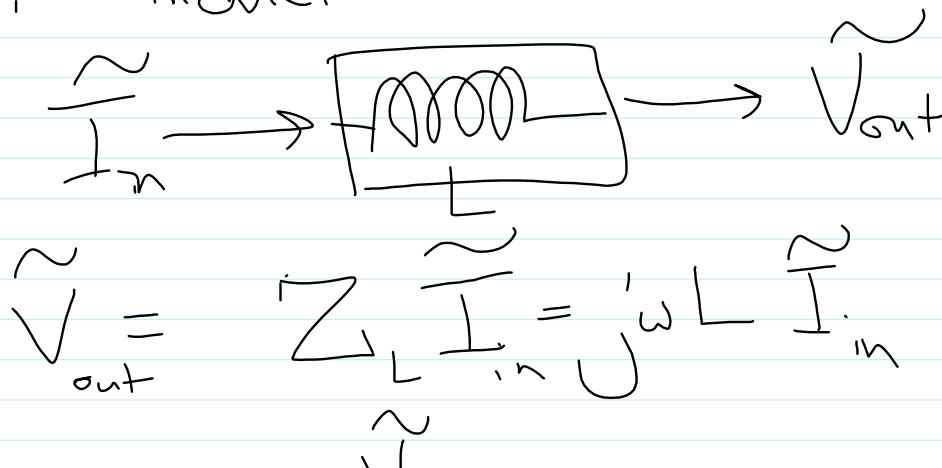
← factored form

} general form

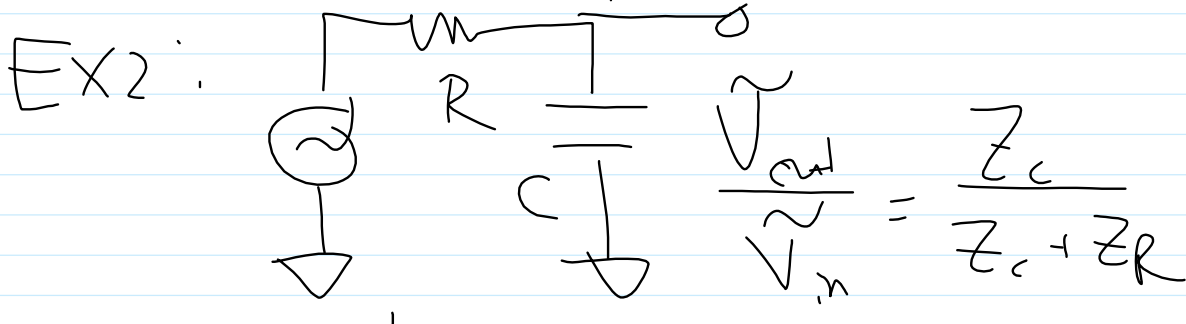
Transfer functions capture input-output behavior

$$H(j\omega) = \frac{\tilde{out}}{\tilde{in}}$$

Ex: inductor



$$Z_L(j\omega) = \frac{V_{out}}{I_{in}} = j\omega L$$



$$H(j\omega) = \frac{j\omega C}{j\omega C + R} \times \frac{j\omega C}{j\omega C} = \frac{1}{1 + j\omega RC}$$

$$= \frac{1}{1 + j\omega \frac{1}{RC}} \quad \frac{1}{RC} = \omega_p$$

From transfer func
to Bode plots, ~

$H(j\omega)$ is a complex number
 \Rightarrow has magnitude $|H(j\omega)|$
 and phase $\angle H(j\omega)$

$$H(j\omega) = |H(j\omega)| e^{j \angle H(j\omega)}$$

\Rightarrow helpful to plot $|H(j\omega)|$ and

$\angle H(j\omega)$ as fns of ω

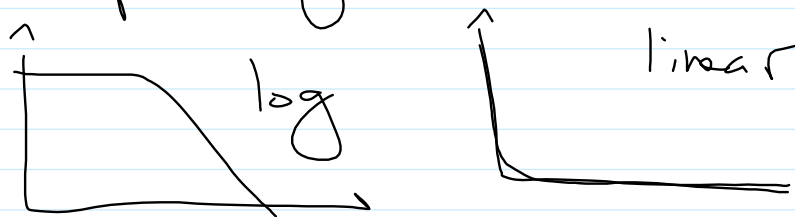
→ Bode plot

II. Bode Plot Intro

- 1) log-log for magnitude $|H(j\omega)|$
- 2) log-linear scale for phase $\angle H(j\omega)$

Why?

- changes in $|H|$, $\angle H$ happen over huge range of ω (orders of magnitude)
- Magnitude also changes over orders of magnitude



phase → doesn't change so much
(LPF: $0^\circ \rightarrow -90^\circ$)

⇒ log-linear

* log scale makes plotting easier!

$$H(j\omega) = \frac{H_{z_1}(j\omega) H_{z_2}(j\omega) \dots}{H_{p_1}(j\omega) H_{p_2}(j\omega) \dots}$$

$$|z_1 z_2| = |z_1| |z_2|$$

$$|H(j\omega)| = \frac{|H_{z_1}(j\omega)| |H_{z_2}(j\omega)| \dots}{|H_{p_1}(j\omega)| |H_{p_2}(j\omega)| \dots}$$

Amazing to plot!

But in log scale ...

$$\log AB = \log A + \log B$$

$$\log(A/B) = \log A - \log B$$

$$\log |H(j\omega)| = \log |H_{z_1}(j\omega)| + \log |H_{z_2}(j\omega)| + \dots \\ - \log |H_{p_1}(j\omega)| - \log |H_{p_2}(j\omega)| - \dots$$

We can break up transfer fn into smaller constituent parts

~~***~~ This is powerful, because ~~***~~

we can use smaller constituent plots we already know to get



* What about phase?

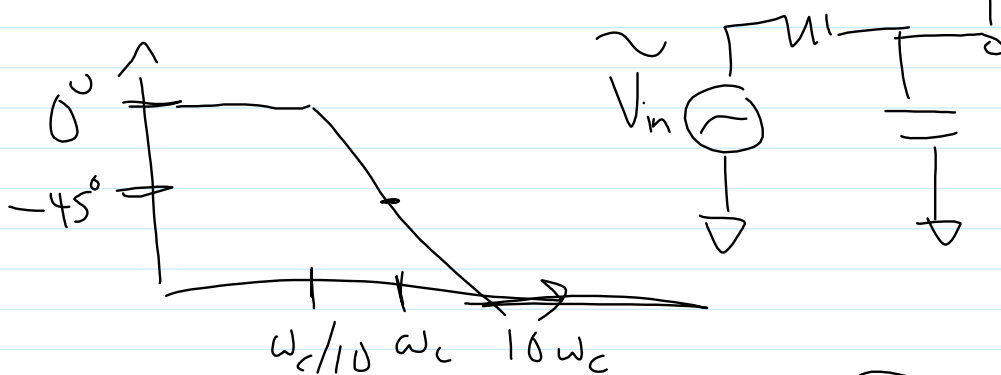
$$\angle \frac{z_1}{z_2} = \frac{\angle |z_1| e^{j\theta_1}}{|z_2| e^{j\theta_2}} = \angle e^{j(\theta_1 - \theta_2)}$$

$$= \theta_1 - \theta_2 = \angle z_1 - \angle z_2$$

$$\angle z_1 z_2 = \angle e^{j\theta_1} e^{j\theta_2} = \angle e^{j(\theta_1 + \theta_2)}$$

$$= \theta_1 + \theta_2 = \angle z_1 + \angle z_2$$

Play the same trick; add and subtract constituent plots!



III. Plotting Bode Plots

Given factored form of transfer fn;

① Draw out Bode plots for each component \Rightarrow table

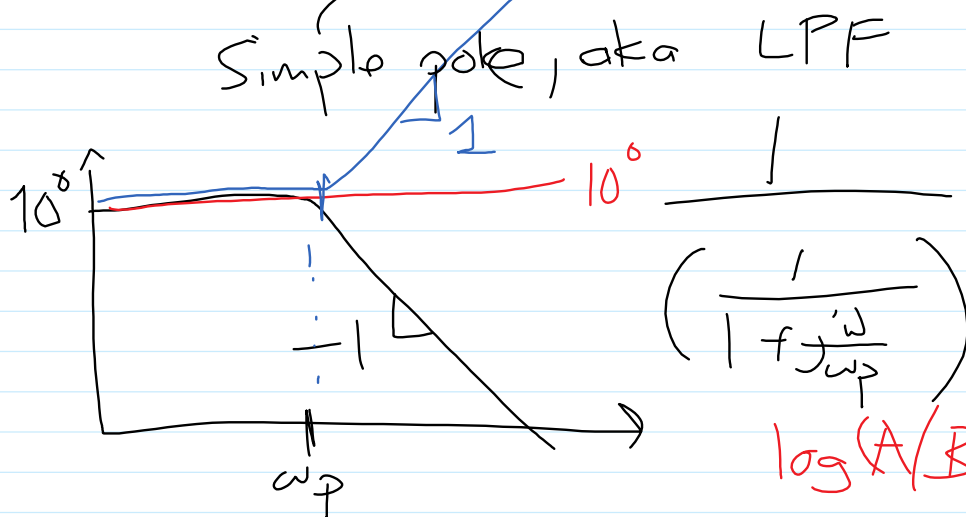
② Add the plots together!
 - b/c log, exponent properties

Ex 1: $1 + \frac{j\omega}{\omega_p} = H'(j\omega)$

↑ magnitude ↑ phase

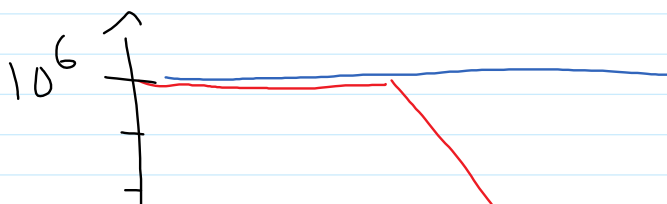
("simple zero")

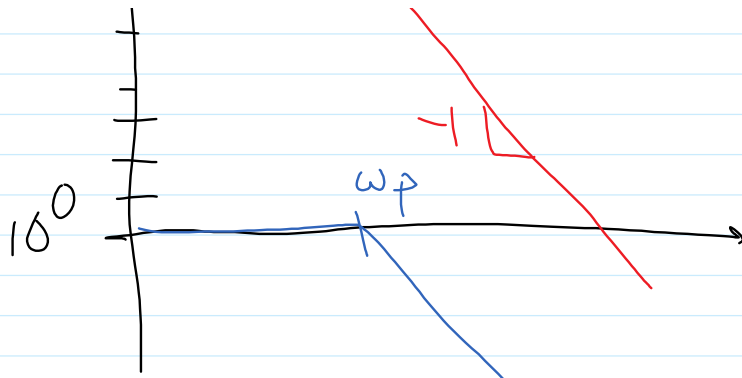
$$H'(j\omega) = \frac{1}{1 + \frac{j\omega}{\omega_p}} = \frac{1}{H(j\omega)}$$



$$\log(A/B) = \log A - \log B$$

Ex 2: $H(j\omega) = 10^6 \frac{1}{1 + \frac{j\omega}{\omega_p}}$





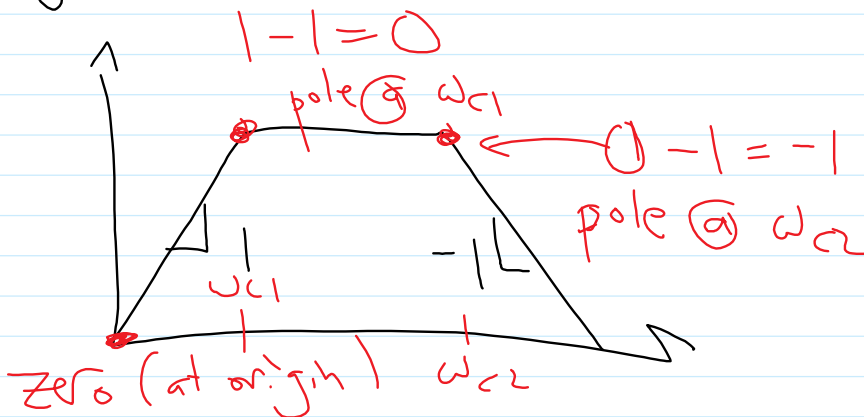
IV. Reading Bode Plots

— yesterday, we built intuition that pole ω_p is where slope goes down

— zero does the opposite

slope goes down by -1 \implies pole at that value ω_p

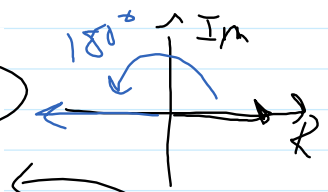
slope goes up by $+1$ \implies zero at that value ω_z



Dis 2D Worksheet

Wednesday, July 1, 2020 4:36 PM

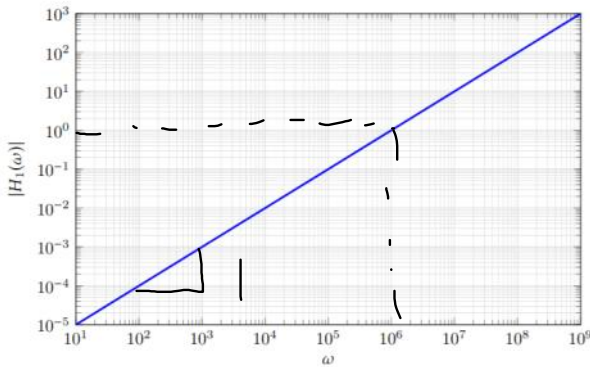
Factor	Bode Magnitude	Bode Phase
Constant K	$20 \log K$ 0 dB	$\pm 180^\circ$ if $K < 0$ 0° if $K > 0$ $(00N)^\circ$
Zero @ Origin $(j\omega)^N$	slope = $20N$ dB/decade	0°
Pole @ Origin $(j\omega)^{-N}$	slope = $-20N$ dB/decade	$(-90N)^\circ$
Simple Zero $(1 + j\omega/\omega_c)^N$	slope = $20N$ dB/decade	0° to $(90N)^\circ$
Simple Pole $(\frac{1}{1 + j\omega/\omega_c})^N$	slope = $-20N$ dB/decade	0° to $(-90N)^\circ$
Quadratic Zero $[1 + j2\zeta\omega/\omega_c + (j\omega/\omega_c)^2]^N$	slope = $40N$ dB/decade	0° to $(180N)^\circ$
Quadratic Pole $\frac{1}{[1 + j2\zeta\omega/\omega_c + (j\omega/\omega_c)^2]^N}$	slope = $-40N$ dB/decade	0° to $(-180N)^\circ$



$20N$ dB/decade
 \downarrow
 N orders of magnitude per decade
 \downarrow
 slope of N

1 Bode Plot Practice

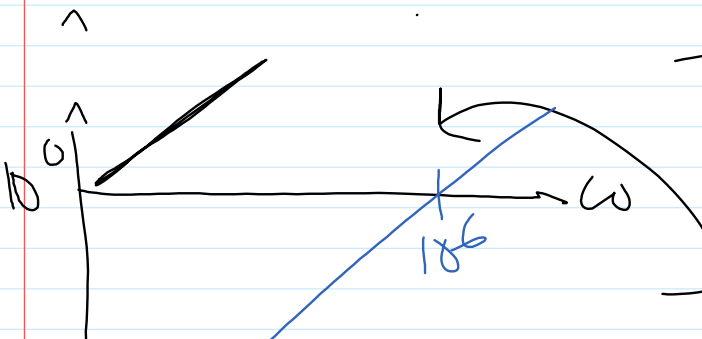
a) Identify the locations of the poles and zeroes in the following magnitude Bode plot. What transfer function $H_1(\omega)$ would result in this plot?

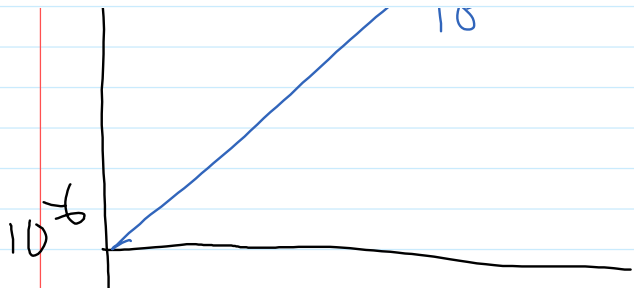


- slope is going up
 \Rightarrow zero
 $|j\omega| = \omega \rightarrow$ goes up
 ω (pos. slope)

- slope is 1
 \Rightarrow single zero

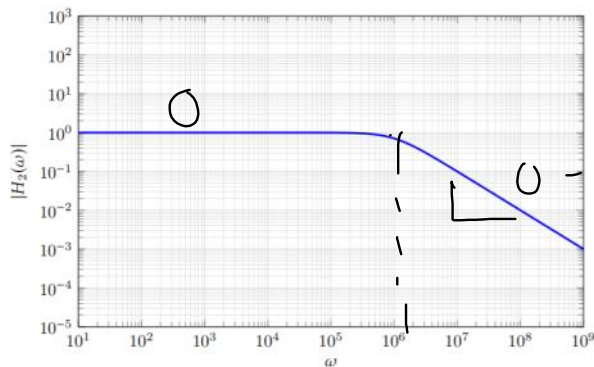
- Doesn't look like it ever goes flat
 \Rightarrow zero at origin
 - $|H_1(10^6)| = 1$





$|H_1(j10^6)| = 1$
 $\Rightarrow H_1(j10^6) = \frac{j\omega}{10^6}$

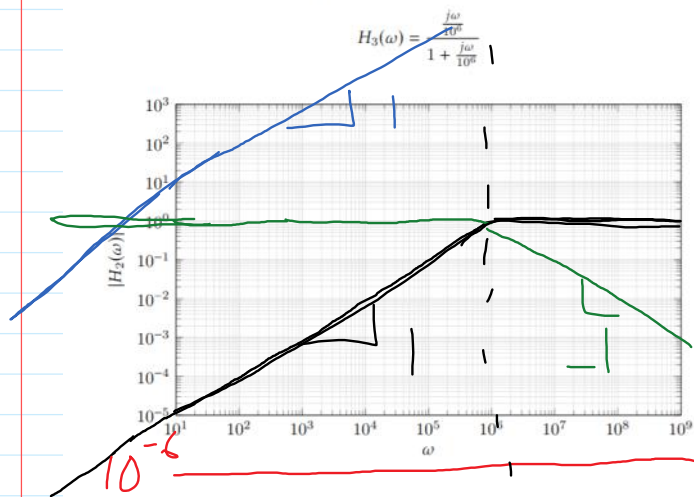
b) Identify the locations of the poles and zeroes in the following magnitude Bode plot. What transfer function $H_2(\omega)$ would result in this plot?



- initially $|H| = 1$,
 scaling is 1
 - goes down by 1
 \Rightarrow pole at 10^6

$$H_2(\omega) = \frac{1}{1 + j\frac{\omega}{10^6}}$$

c) Identify the locations of the poles and zeroes in the following transfer function. Then sketch the magnitude Bode plot.



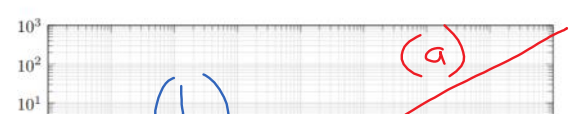
Method: table!

$$H_3(\omega) = \frac{1}{10^6} \times (j\omega) \times \frac{1}{1 + j\frac{\omega}{10^6}}$$

High Pass filter!

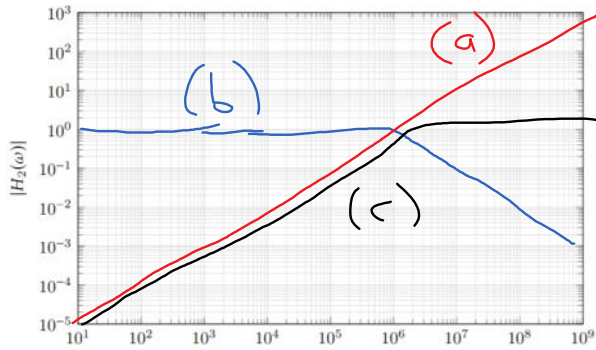
c) Identify the locations of the poles and zeroes in the following transfer function. Then sketch the magnitude Bode plot.

$$H_3(\omega) = \frac{j\omega}{1 + j\frac{\omega}{10^6}}$$



Alternative!

Notice $(c) = (a) \times (b)$

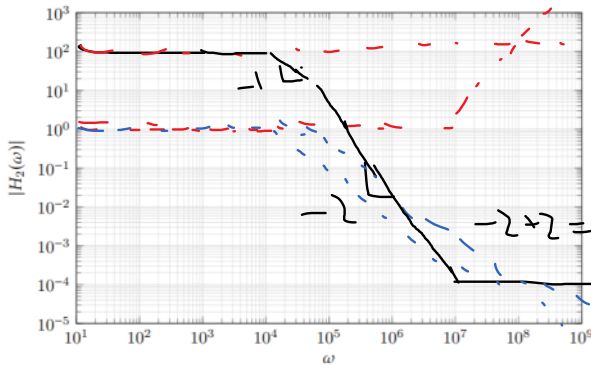


Notice $(c) = (a) \times (b)$

d) Identify the locations of the poles and zeroes in the following magnitude Bode plot. Then sketch the magnitude Bode plot.

$$H_4(\omega) = 100 \frac{(1 + \frac{j\omega}{10^7})^2}{(1 + \frac{j\omega}{10^4})(1 + \frac{j\omega}{5 \times 10^4})}$$

Find ω_p 's, ω_z 's!



$$H_4(\omega) = 100 \times \left(1 + \frac{j\omega}{10^7}\right) \left(1 + \frac{j\omega}{10^7}\right) \times \frac{1}{\left(1 + \frac{j\omega}{10^4}\right)} \times \frac{1}{\left(1 + \frac{j\omega}{5 \times 10^4}\right)}$$

zeros: 2 at

$$\omega_z = 10^7 \text{ rad/s}$$

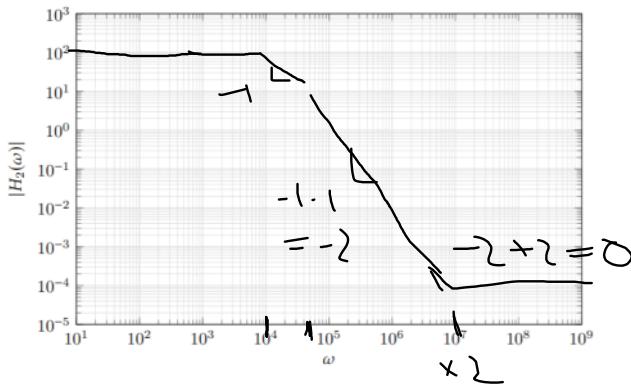
$$\text{poles: } \omega_{p1} = 10^4 \text{ rad/s}$$

$$\omega_{p2} = 5 \times 10^4 \text{ rad/s}$$

$$K = 100 = 10^2$$

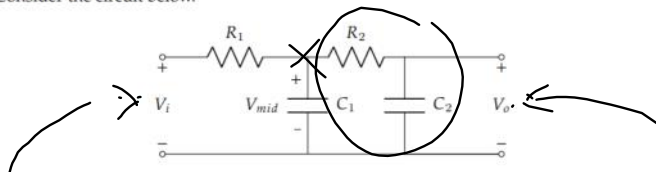
d) Identify the locations of the poles and zeroes in the following magnitude Bode plot. Then sketch the magnitude Bode plot.

$$H_4(\omega) = 100 \frac{(1 + \frac{j\omega}{10^7})^2}{(1 + \frac{j\omega}{10^4})(1 + \frac{j\omega}{5 \times 10^4})}$$



2 Transfer functions and why loading is annoying

Consider the circuit below.



The circuit has an input phasor voltage \bar{V}_i at frequency ω rad/sec applied at the input terminals shown in the illustration above, causing an output phasor voltage \bar{V}_o at output terminals.

a) We are going to construct the transfer function $H(\omega) = \frac{\bar{V}_o}{\bar{V}_i}$ in two steps. We will

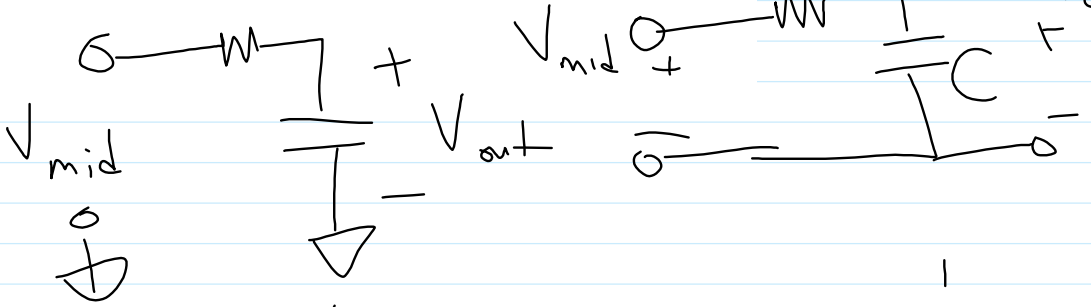
$$H(\omega) = \frac{\bar{V}_o}{\bar{V}_i}$$

$$H(\omega) = \frac{\bar{V}_o}{\bar{V}_i}$$

terminals shown in the illustration above, causing an output phasor voltage \tilde{V}_o at output terminals.

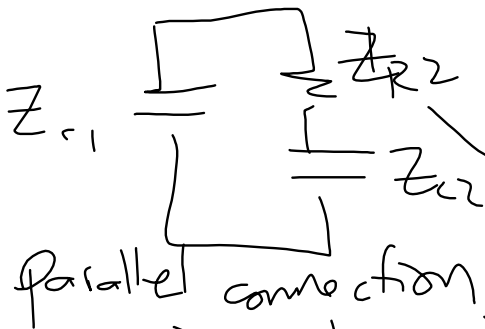
a) We are going to construct the transfer function $H(\omega) = \frac{\tilde{V}_o}{\tilde{V}_i}$ in two steps. We will compute two intermediate transfer functions, $H_1(\omega) = \frac{\tilde{V}_{mid}}{\tilde{V}_i}$ and $H_2(\omega) = \frac{\tilde{V}_o}{\tilde{V}_{mid}}$. Then, we will find the overall transfer function as the product of these two intermediate transfer functions, i.e. $H(\omega) = \frac{\tilde{V}_o}{\tilde{V}_i} = H_1(\omega)H_2(\omega)$. This approach is valid since the \tilde{V}_{mid} cancel. For the first step, find the intermediate transfer function $H_2(\omega) = \frac{\tilde{V}_o}{\tilde{V}_{mid}}$. Have your expression be in terms of Z_{R2} and Z_{C2} , that is the impedances of R_2 and C_2 .

$$H_2(j\omega) = \frac{\tilde{V}_o}{\tilde{V}_{mid}}$$



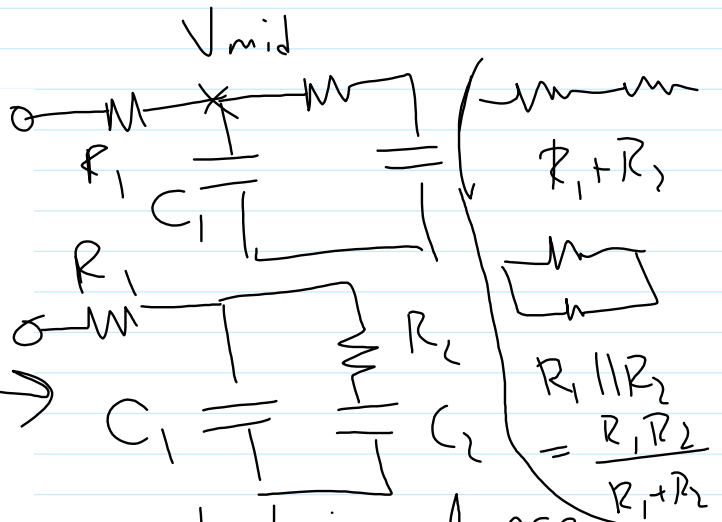
$$\frac{\tilde{V}_{out}}{\tilde{V}_{mid}} = \frac{Z_{C2}}{Z_{C2} + Z_{R2}} = \frac{1}{j\omega C_2 R + \frac{1}{j\omega C_2}} = \frac{1}{1 + j\omega R_2 C_2}$$

b) Now, compute the other intermediate transfer function $H_1(\omega) = \frac{\tilde{V}_{mid}}{\tilde{V}_i}$. Have your expression be in terms of Z_{R1} , Z_{R2} , Z_{C1} , and Z_{C2} . (i.e. Don't forget to consider the impact of loading by R_2 and C_2 in this transfer function.)



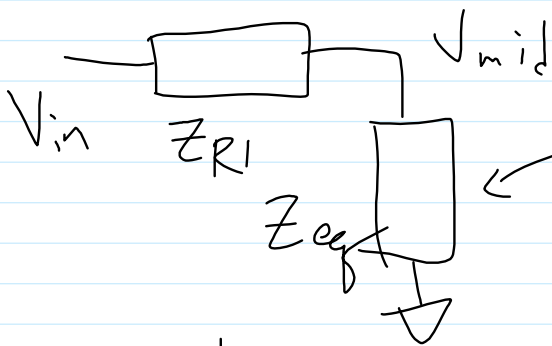
parallel connection!

collapse into equivalent impedance



$$R_1 + R_2$$

$$R_1 \parallel R_2 = \frac{R_1 R_2}{R_1 + R_2}$$



$$Z_{eq} = Z_{C1} \parallel (Z_{C2} + Z_{R2})$$

$$\frac{\tilde{V}_{mid}}{\tilde{V}_i} = \frac{Z_{eq}}{Z_{R1} + Z_{eq}} = \frac{\left(\frac{1}{j\omega C_1}\right) \parallel \left(\frac{1}{j\omega C_2} + R_2\right)}{\left(\frac{1}{j\omega C_1}\right) \parallel \left(\frac{1}{j\omega C_2} + R_2\right) + R_1}$$

$$\begin{aligned}
 \frac{V_{mid}}{V_{in}} &= \frac{Z_{eq}}{Z_{eq} + Z_{R1}} = \frac{(j\omega C_1 \parallel j\omega C_2)}{\left(\frac{1}{j\omega C_1} \parallel \left(\frac{1}{j\omega C_2} + R_2\right)\right) + R_1} \\
 &= \frac{\frac{1}{j\omega C_1} \times \left(\frac{1}{j\omega C_2} + R_2\right)}{\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} + R_2} \times \frac{\left(\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} + R_2\right)}{\left(\frac{1}{j\omega C_2} + \frac{1}{j\omega C_2} + R_2\right)} \\
 &= \frac{\frac{1}{j\omega C_1} \times \left(\frac{1}{j\omega C_2} + R_2\right)}{\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} + R_2} + R_1 \frac{\left(\frac{1}{j\omega C_2} + \frac{1}{j\omega C_2} + R_2\right)}{\left(\frac{1}{j\omega C_2} + \frac{1}{j\omega C_2} + R_2\right)} \\
 &= \frac{\left(\frac{1}{j\omega C_2} + R_2\right) \frac{1}{j\omega C_1}}{\left(\frac{1}{j\omega C_2} + R_2\right) \frac{1}{j\omega C_1} + R_1 R_2 + \frac{R_1}{j\omega C_1} + \frac{R_2}{j\omega C_2}} \times \frac{(j\omega C_1)(j\omega C_2)}{(j\omega C_1)(j\omega C_2)} \\
 &= \frac{j\omega C_2 \left(\frac{1}{j\omega C_2} + R_2\right)}{\left(\frac{1}{j\omega C_2} + R_2\right) j\omega C_2 + (j\omega)^2 R_1 R_2 C_1 C_2 + j\omega C_2 R_1 + j\omega C_1 R_2} \\
 \Rightarrow H_1(\omega) &= \frac{1 + j\omega R_2 C_2}{1 + j\omega(R_1 C_1 + R_2 C_2 + R_1 C_2) + (j\omega)^2 R_1 R_2 C_1 C_2}
 \end{aligned}$$

c) Then, use these two intermediate transfer functions to calculate the overall transfer function as $H(\omega) = \frac{\tilde{V}_o}{\tilde{V}_i} = H_1(\omega)H_2(\omega)$.

$$H(j\omega) = \frac{1}{1 + j\omega(R_1C_1 + R_2C_2 + R_1C_2) + (j\omega)^2 R_1R_2C_1C_2}$$

d) Sometimes it is useful to collect all the frequency dependence into one place and to figure out how to think about what scale might be somewhat natural for the frequency. Obtain an expression for $H(\omega) = \tilde{V}_o/\tilde{V}_i$ in the form

$$H(\omega) = \frac{\tilde{V}_o}{\tilde{V}_i} = \frac{1}{1 + 2\xi \frac{j\omega}{\omega_c} + \frac{(j\omega)^2}{\omega_c^2}}$$

given that $R_1 = 2\Omega$, $R_2 = 4\Omega$, $C_1 = \frac{9}{2}F$, and $C_2 = 1F$. What are the values of ξ and ω_c ?

$$R_1C_1 = 2\Omega \times \frac{9}{2}F = 9s$$

$$R_2C_2 = 4\Omega \times 1F = 4s$$

$$R_1C_2 = 2\Omega \times 1F = 2s$$

$$\Rightarrow H(j\omega) = \frac{1}{1 + 15j\omega + (j\omega)^2 36} \quad \leftarrow \begin{aligned} \omega_c^2 &= \frac{1}{36} \\ \omega_c &= \frac{1}{6} \end{aligned}$$

$$\xi = \frac{5}{4}, \quad \omega_c = \frac{1}{6} \text{ rad/s}$$

e) For the previous case, what is the magnitude of the transfer function at the $\omega = \omega_c$ you calculated? \leftarrow corner freq
This is here so that you can see that just because we called it ω_c doesn't mean that the amplitude here is $\frac{1}{\sqrt{2}}$.

$$H(\omega) = \frac{1}{1 + 2\xi \frac{j\omega_c}{\omega_c} + \frac{(j\omega_c)^2}{\omega_c^2}} \leftarrow -1$$

$$= \frac{1}{2\xi j}$$

$$|H(\omega_c)| = \frac{1}{2\xi} = \frac{1}{2} \times \frac{1}{5} = \frac{1}{10} = 0.1$$

quadratic \Rightarrow we would expect $\frac{1}{(1+j\frac{\omega}{\omega_c})^2} \xrightarrow{\omega=\omega_c} \frac{1}{(1+j)^2}$

$$\left| H_{\text{perf}}(\omega_c) \right|_{\text{quadratic}} = \frac{1}{\|1+2j\|} = \underline{\underline{\frac{1}{2}}}$$

B/c of loading, $|H(\omega_c)| \neq |H_{\text{perf}}(\omega_c)|_{\text{quad}}$

f) We can express the transfer function $H(\omega)$ in the polar form. That is,

$$H(\omega) = M(\omega)e^{j\phi(\omega)}$$

The functions $M(\omega)$ and $\phi(\omega)$ are the magnitude and the phase angle of $H(\omega)$, respectively. Write down $M(\omega)$ and $\phi(\omega)$ using the transfer function you derived in part (b).

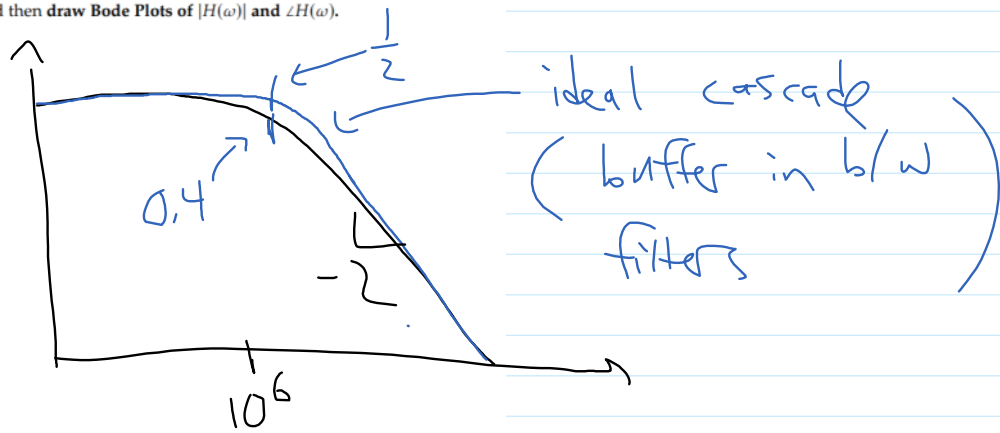
$$H(j\omega) = \frac{1}{1 + 15j\omega - 36\omega^2} \quad \left| \frac{z_1}{z_2} \right| = \frac{|z_1|}{|z_2|}$$

$$M(\omega) = |H(j\omega)| = \frac{1}{\sqrt{(1-36\omega^2)^2 + (15\omega)^2}}$$

$$\begin{aligned} 1 + 15j\omega - 36\omega^2 &= (1 - 36\omega^2) + j(15\omega) \\ &= x + jy \end{aligned}$$

$$\begin{aligned} \angle H(j\omega) &= \angle \left(\frac{1}{(1 - 36\omega^2) + j(15\omega)} \right) \\ &= 0 - \angle \left((1 - 36\omega^2) + j(15\omega) \right) \\ &= \underline{\underline{-\arctan \left(\frac{15\omega}{1 - 36\omega^2} \right)}} \end{aligned}$$

g) Use a computer and then draw Bode Plots of $|H(\omega)|$ and $\angle H(\omega)$.



$$\zeta = 0, H(\omega_c) = \frac{1}{2\zeta\omega_c} = \frac{1}{0} \rightarrow \infty$$

